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SUBJECT NAME : DESIGN LAB MANUAL

SUBJECT CODE : 17MEL76

SEMESTER : VII

EXPERIMENT NO:1
CRITICAL OR WHIRLING OR WHIPPING SPEED OF SHAFT

AIM: To determine the critical speed of a shaft or whirling speed of a shaft.

APPARATUS: Stop clock, Tachometer and Weights (optional)

THEORY:

The speed at which the rotating shaft varies violently in transverse direction is called the "critical or whirling speed "

Or

When the speed of shaft is equal to natural frequency of vibration such a frequency is called as critical or whirling or whipping speed.

If the body or a disc mounted upon the shaft rotates about it, then C.G. of the disc must be at the shaft axis, if perfect running balance is to be obtained. But practically because of difficulty of perfect machining of disc (rotor) C.G does not coincide with shaft axis. Hence, when such shaft rotates, it deflects towards heavier side of the disc due to unbalanced centrifugal force. As the speed increases the shaft vibrates violently upto resonance speed, and after resonance speed the shaft again runs smoothly.

CRITICAL SPEED DEPENDS UPON THE FOLLOWING FACTOR:

1.Length of the shaft

2.Diameter of the shaft

3.Bearing supports conditions i.e. fixed or free.

4.The magnitude of the load.

5.The location of the load carried by the shaft

PROCEDURE:

1) Fix the required shaft at the driving end.
2) Fix the Bearing block at tail end (either for fixed end condition or free end condition) And tighten the shaft

3) Start the motor and slowly increase the speed at certain speed discs will be vibrating Violently and note down the speed of shaft.
4) Increase the speed now shaft is operating above critical speed without vibration.
5) Repeat the procedure by changing shaft.

SPECIFICATION:

1. Shaft diameter = ……………m
2. Bearing block
   a. Driving end: - Fixed end shaft supported with two Bearing
   b. Tail end: - Fixed end support with self-aligning ball Bearing
   c. Young's modulus of the shaft =…………N/m^2
   d. Length of the shaft =…………m
3. Moment of inertia of the shaft =……….. m^4
4. Uniformly Distributed Load
   i. = 0.064 kg/m for 3.17 mm diameter shaft.
   ii. = O.138 kg/m for 4.75 mm diameter shaft
   iii. = O.248 kg/m for 6.35 diameter shaft
5. Density of the shaft material (ρ) ………..Kg/m^3

FORMULAE:

a. For bending mode:

Angular speed , $\omega = 22a / L^2$

Where, $a = \sqrt{EI/A\rho}$, ρ = Mass/ Volume, (Kg/m^3),Critical speed, $N = \omega \times 60 / 2\pi$

b. For twisting mode:

Angular speed, $\omega = 61.7\, a / L^2$

Critical speed, $N = \omega \times 60 / 2\pi$

TABULAR COLUMN:

Sl.No	Diameter of shaft 'mm'	Length of shaft 'm'	Critical speed, N rpm			
			Bending mode		Twisting mode	
			Theoretical	Experimental	Theoretical	Experimental
1	3.17	830	1394.00	1450.00	3910.00	3400.00
2	4.75	830	2100.00	2000.00	5392.00	4100.00
3						
4						

CALCULATION:

For shaft

- Diameter = 3.17 mm, Length= 830mm and Mass, M = 0.064 kg/m
- Young's Modulus the shaft = 207 Gpa
- Area, $A = \pi d^2 / 4 = \pi (0.00317)^2 / 4 = 7.892 \times 10^{-6} m^2$
- Moment of inertia, $I = \pi d^4 / 64 = \pi (0.00317)^4 / 64 = 4.9568 \times 10^{-12} m^4$
- Density, ρ = Mass/ Volume, (Kg/m^3), Volume=A X L,
- $a = \sqrt{EI/A\rho}$, = 4.004

a. For bending mode:

Angular speed , $\omega = 22a / L^2$ = 127.86 rad/Sec

Critical speed, $N = \omega \times 60 / 2\pi$ = 1394.00 rpm

b. For twisting mode:

Angular speed, $\omega = 61.7 a / L^2$ = 358.61 rad/sec

Critical speed, $N = \omega \times 60 / 2\pi$=3910.00 rpm

EXPERIMENT: 2

PORTER GOVERNOR

AIM: To determine the theoretical lift, friction and controlling of the governor.

APPARATUS: universal governor experimental set-up, tachometer set of masses.

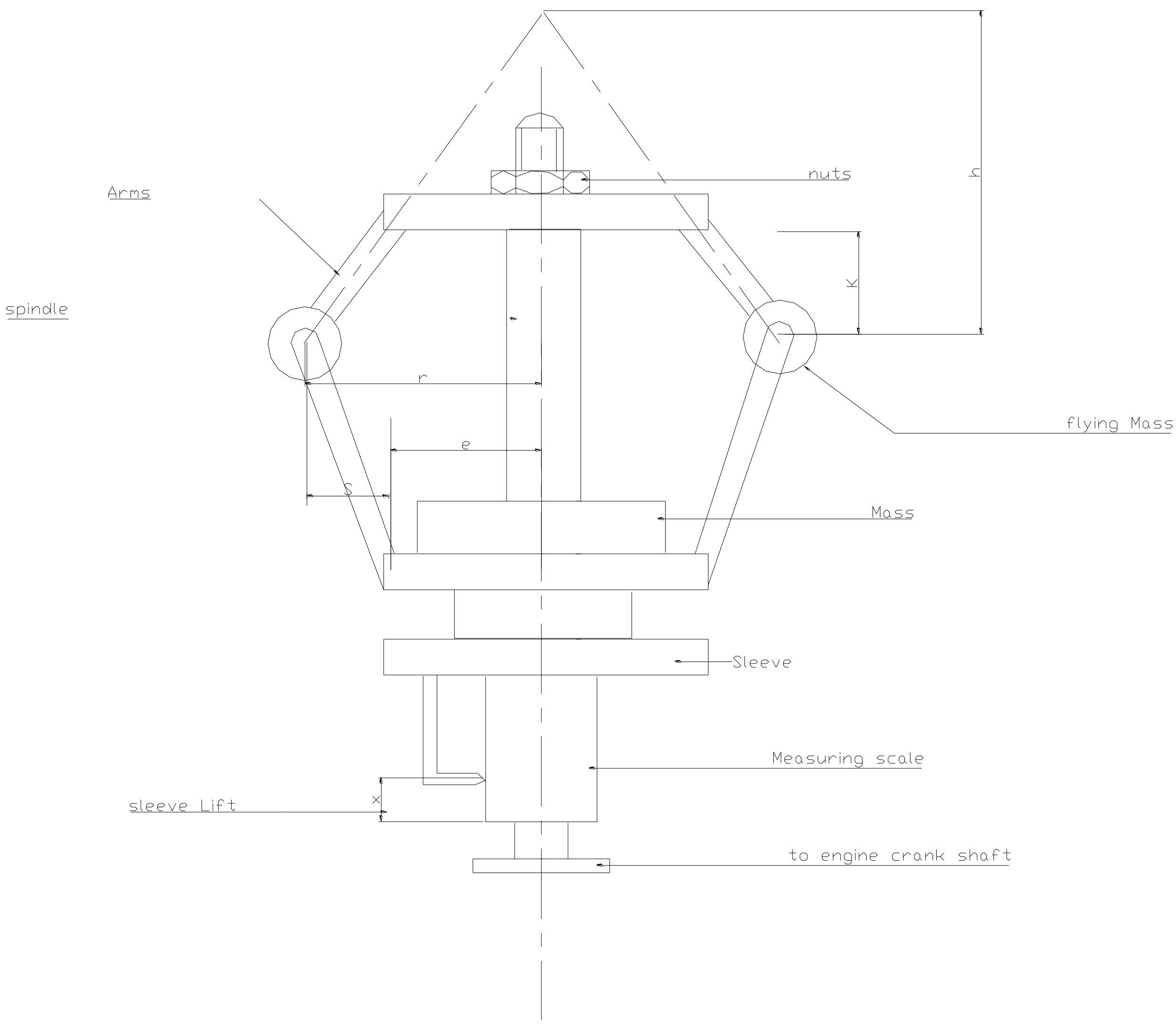
PROCEDURE:

1. Place the porter governor assembly over the spindle of the universal governor apparatus
2. Place the required load on the spindle
3. Tighten the bolts and nuts
4. Start the motor adjust the speed to the required value
5. Note down the sleeve rise (lift) and also the speed
6. Repeat the experimental procedure for different loads and different speeds

SPECIFICATION: -

- Length of each Link = L = mm
- Distance of top link from bottom link 2k = 0.216m = $2k_0$
- Height of balls where central lines intersect with the axis of rotation h = 0.195 m =h_0
- Initial radius of rotation r_0 = 0.1125 m = r
- Mass of sleeve assembly M = 2.14 kgs.
- Weight of sleeve assembly W = N
- Mass of one side balls m_b = 0.4kgs.
- Weight of one side balls w_b = N

EXPERIMENTAL SET UP:



TABULAR COLUMN:

Sl.No	Mass of Sleeve 'kg"	Masses added to Sleeve 'kg'	Total mass'M' 'kg'	Governor speed 'N' rpm'	Sleeve lift 'h' 'cm'		Controlling force 'fc' 'N'	Frictional force 'F' 'N'
					Experimental	Theoretical		
1	2.14	0	2.14	186	1.5	1.6	17.14	$4x10^{-3}$
2	2.14	0.4	2.54	195	1.5	2.2	13.17	2.52
3	2.14	0.8	2.94	206	1.5	2.0	23.82	2.530
4	2.14	1.2	3.34	215	1.5	2.0	25.95	2.53

FORMULAE :

- Lift = $h_1 = [(m_b g + Mg)/m_b]\ 1/N^2 * (60/2\pi)^2$
- $L^2 = \{[h_1^2/(0.05 + s_1)^2] + 1\}\ s_1^2$
- $k_1 = \sqrt{L^2 - s_1^2}$, $x_1 = 2(k_0 - k_1)$
- Controlling force: $Fc = m_b\ \omega_1^2 r_1$, where $r_1 = 0.05 + s_1$
- Frictional force = $h1 = \{w_b + (w \pm F)/m_b\}\ 1/N^2 * (60/2\pi)^2$

CALCULATION:

- Lift = $h_1 = [(m_b\, g + Mg/m_b)]\ 1/N^2 * (60/2\pi)^2$

  $h_1 = \{(0.4 * 9.81 + 2.14 * 9.81)\}/(186)^2 * (60/2\pi)^2$

  $h_1 = 0.164$ m

- $L^2 = \{[h_1^2/ (0.05 + s_1)] + 1\}\ s_1^2$

  $0.0156 = \{(0.164)^2 / (0.05 + s_1)^2 * 1\}\ s_1^2$

  By trial & error, $s_1 = 0.075$m

- $k_1 = \sqrt{L^2 - s_1^2}$

  $k_1 = 0.1$m

- $x_1 = 2(k_0 - k_1)$

  $x_1 = 2(0.108-0.1) = 0.016$m

- $Fc = m_b\, \omega_1^2 r_1$

  $Fc = 0.4(18.84)^2 0.125 = 17.74$ N

- Frictional force = $h_1 = \{w_b + (w \pm F) /m_b\}\ 1/ N^2 * (60/2\pi)^2$

  $0.164 = \{0.4+(2.14\pm F)/0.4\}*9.81*1/186^2*(60/2\pi)^2$

  $F = \pm 4x10^{-3}$ N

GRAPHS:

I) Controlling force v/s radius of rotation

II) Controlling force v/s speed

EXPERIMENT: 3

HARTNELL GOVERNOR

AIM: To determine the theoretical lift, friction and controlling of the governor.

APPARATUS: universal governor experimental set-up, tachometer set of masses springs of different stiffness.

PROCEDURE:

1. Mount the given Hartnell governor assembly over the spindle.
2. Tighten the necessary nuts and Bolts.
3. Start the motor and adjust the speed.
4. The flyweight's fly outwards due to centrifugal force, the sleeve will raise.
5. Measure the sleeve and sleeve raise.
6. Repeat the experiments at different speeds spring forces over the sleeve by changing the initial compressions and springs of different stiffness of the governor.
7. Calculate the lift, friction and controlling force of the governor.

SPECIFICATIONS: -

- Motor speed = 1500 rpm.
- Stiffness of spring = 490 N/m and 980 N/m
- Length of the ball arm = 'a' = 0.07m
- Length of the sleeve arm = 'b' = 0.116m
- Mass of one side balls = 'm_b' = 0.196 kg
- Initial radius of rotation of balls = 'r_0' = 0.153m

- Mass of sleeve only = 2.14 kg

FORMULAE:

1. To find lift:-$m_b \omega^2 r$ = b/a { w + k (x+d) }

   where r = (a/b * x) + r_0

2. To find friction :-$m_b \omega^2 r$

   = b/a { w + k (x+d) } ± F

3. To find controlling force

   $Fc = m_b \omega^2 r$

TABULAR COLUMN:

Sl. No	Stiffness of the spring 'K' N/m	Mass of Sleeve 'kg'	Weight of the sleeve 'W' N	Initial length of the spring 'm'	Final length of the spring 'm'	Diff between the spring length 'd' 'm'	Gov speed 'Rpm'	Exp	Theo	Controlling force 'fc' 'N'	Frictional force 'F' 'N'
1	980	2.14	20.99	20.5	20.5	0	265	1	0.724	46.52	0.01643
2	980	2.14	20.99	20.5	20.5	0	298	2	1.618	61.06	5.94E-3
3	980	2.14	20.99	20.5	18	2.5	336	1	0.5	78.86	3.2E-4
4	980	2.14	20.99	20.5	18	2.5	336	2	1.312	86.69	8.45E-3

CALCULATION:

1. **To find lift:-**

- $m_b \omega^2 r$ = b/a { w + k (x+d) } where r = (a/b * x) + r_0

[(2* 0.190) (2*Π * 265 / 60 $)^2$ *0.1590]= [{20.99 +(X_1 +0) *980} (0.116/0.07)]

X_1 = 0.724 cm

2. **To find friction :-**

- ($m_b \omega^2 r$)= = [b/a { w + k (x+d) } ± F]

[(2* 0.190) (2*Π * 265 / 60 $)^2$ *0.1590] = [{20.99 +(X_1 +0) *980} (0.116/0.07) ± F]

F = 0.01643 N

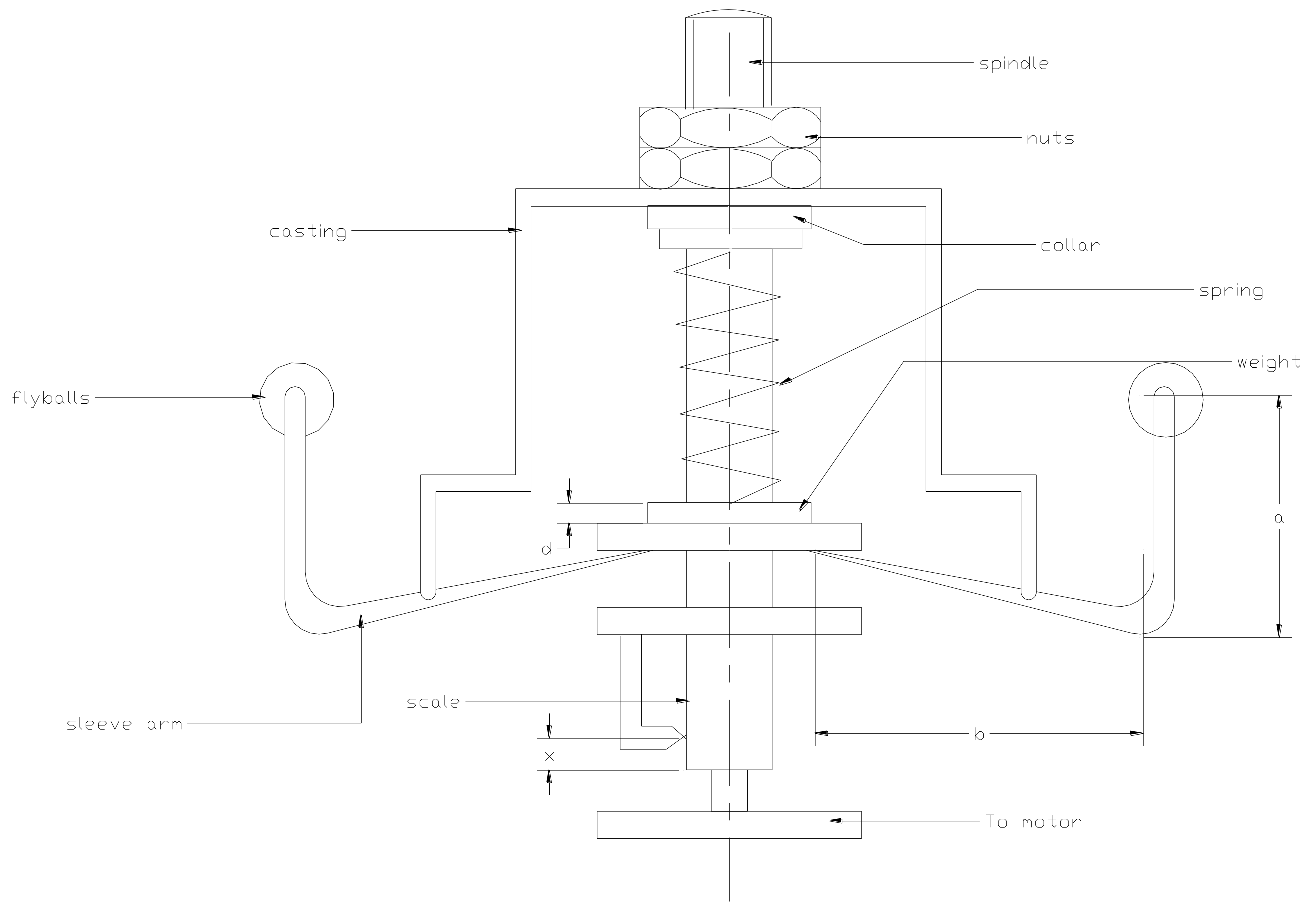
3. **To find controlling force**

- Fc = $m_b \omega^2 r$

Fc = (2* 0.190) (2*Π * 265 / 60 $)^2$ 0.1590

= 46.52 N

EXPERIMENTAL SET UP :



GRAPHS:

1. Controlling force v/s speed
2. Controlling force v/s radius of rotation.

EXPERIMENT 4

TORSION VIBRATION (DAMPED)

Aim: -To study the damped torsion vibration of a single rotor system and to determine the damping factor logarithmic decrement.

Apparatus: -Rotor, Descended (penholder)

Procedure: -

1) Fix the shaft at the bracket at the top
2) Attach the rotor, and desender to the shaft
3) Put the damping liquid (oil or water) into the damping reservoir and set the pen holder at suitable position
4) Oscillate the rotor carefully, so that lateral oscillation does not appear.
5) Lift the desender and gently press the pen over the paper and graph of oscillation should be recorded over the paper.
6) Measure height of amplitude from the graph
7) Repeat above procedure by changing depth of immersion in liquid medium.
8) Plot the graph of logarithmic decrement v/s depth of immersion.

FORMULAE:

1) Logarithmic decrement (δ):

$\delta = 1/n \ln (x_0/x_n)$

Where X_0 = Initial amplitude

Xn = amplitude of the n^{th} cycle.

n = number of cycles.

2) Damping factor (ξ):

$\delta = (2 * 3.14 * \xi) / (\sqrt{1-\xi^2})$

Tabular column :

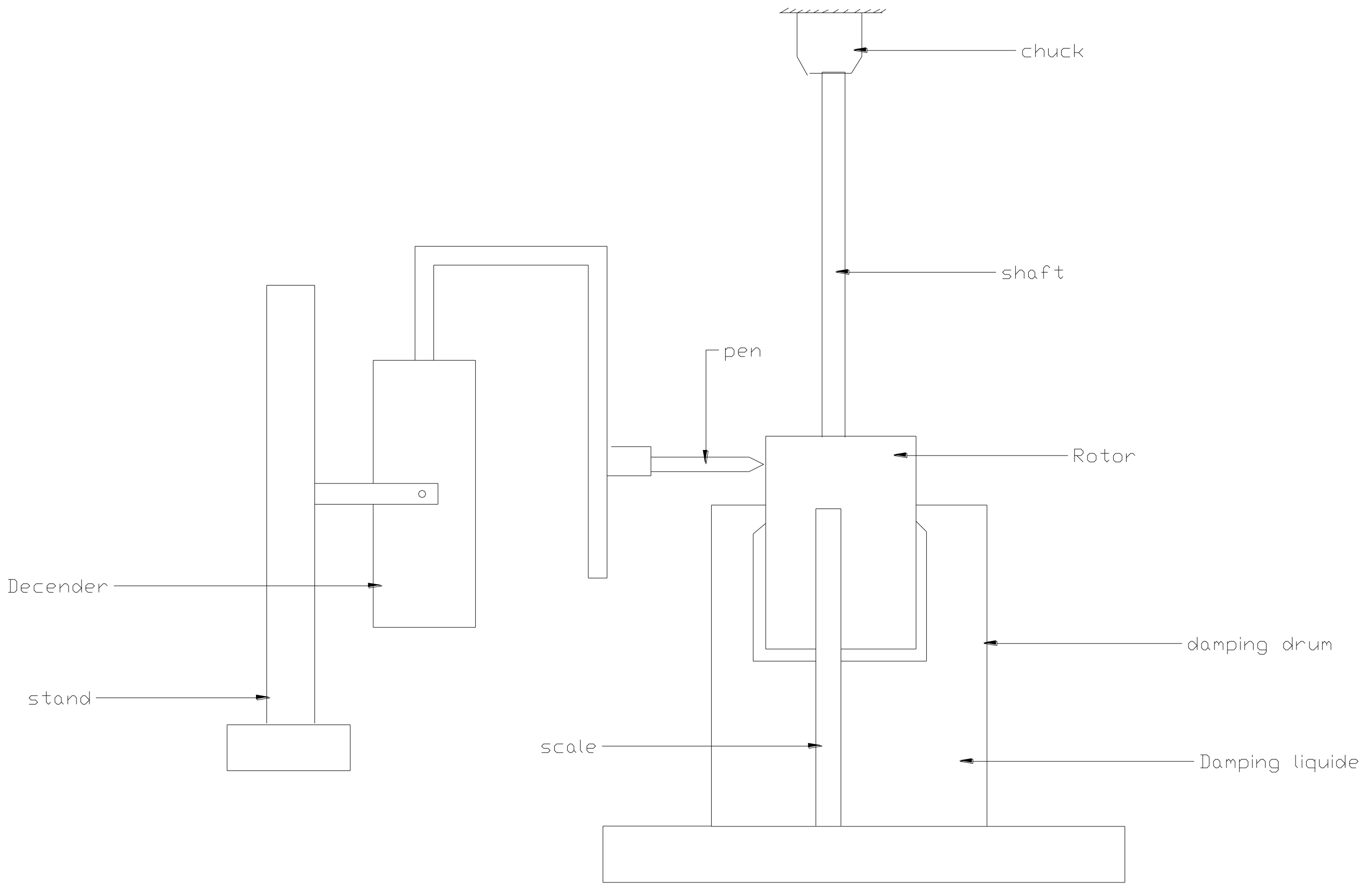
Sl no.	Depth of Immersion in 'mm'	Logarithmic Decrement	Damping factor
1	4	0.152	0.024
2	6	0.086	0.0136
3	8	0.078	0.0124
4			
5			

Specimen calculation:

Depth of immersion: d = 8 cm.

From graph: x_1 = 2.4 cm ; x_n = 1.1 cm ; n = 10 ;

1. $\delta = 1/n \ln(x_1 /x_n) = 1/10 \ln (2.4/1.1) = 0.07$
2. $\xi = (\delta/\sqrt{4\Pi^2 *\delta^2}) = (0.078/\sqrt{4\Pi^2 * 0.078^2}) = 0.0124$


chuck
shaft
pen
Rotor
Decender
damping drum
stand
scale
Damping liquide

EXPERIMENT 5

TORSIONAL VIBRATION (UNDAMPED)

Aim: - To determine frequency of undamped torsional vibration of a single rotor system.

Apparatus: - Stop watch, Single rotor systems.

Procedure: -

1. Fix the rotor at the threaded spindle, fitted in the bearings.
2. Fix the gripping chuck over the spindle
3. Fix the stationary speed bracket at suitable length
4. Thread the shaft through the spindle and tighten the chuck.
5. Oscillate the rotor by hand and measure the time taken for 10 oscillations.
6. Repeat the experiment for different length of the shaft.

Formulae:

1) Experimental frequency $F_n = 1/t_p$

Where t_p = Time period.

2) Theoretical frequency Ft = (1/ 2 * 3.14) * ($\sqrt{GJ/IL}$)

Where G = rigidity modulus of given material

J = polar moment of inertia

I = mass moment of inertia = mk^2

m = mass of rotor

k = radius of shaft.

Tabular column:

SL.no	Length of shaft 'mm"	Time taken for		Frequency	
		10 oscillation Sec	1 oscillation Sec	Expi	Theo
1	0.78	8	0.8	1.25	1.18
2	0.59	7	0.7	1.428	1.357
3	0.29	5	0.5	2.0	1.936
4					
5					

Specimen calculation:

1. F_n(exp) = 1/tp = 1/0.8 = 1.25 Hz.
2. I = $mk^2/2$ =0.01482 kg-m^2
3. G = 0.8*10E11 N/m^2
4. J = Πd^4 / 32 = $\Pi(3*10e\text{-}3)^4$ /32 = 7.952*10e-12 m^4
5. F_n(the)=1/2Π√(GJ/IL)

   =1/2√(0.8*10e11) (7.952*10e12) / (0.014820.78)=

   =1.HZ

EXPERIMENT: 6

STATIC AND DYNAMIC BALANCING OF ROTATING MASSES

Aim: To find static and dynamic balancing rotating masses.

Apparatus: It consists of a frame, which is hang by chains from the main frame. A shaft rotates within bearings in the frame. Four eccentric weights are supplied which can be easily fitted over the shaft. For static balancing one weight is attached and balanced with another weight. For dynamic balancing three or four weights are mounted over the shaft at calculated angle and the shaft is rotated. If the system is unbalanced, vibrations indicate it.

Theory

Balancing of masses is important part of a machine design, when the mass is stationary it can be easily balanced by putting suitable counter weight on the opposite side of mass. When the mass is revolving and if it is left unbalanced, then a centrifugal force is developed which changes its direction during rotation. This causes pre- mature failure of bearings and shafts are unbalanced, hence balancing is essential in machine design.

Procedure:

1) Static balancing:

1) Remove the leather rope over the pulley.
2) Fix the points at 0^0 position.
3) Attach the weight pans on both sides.
4) Remove locking screw and go on putting steel balls in the pan till, the points is turned through 90^0.now the weights is balanced by steel balls count number

of balls. This is relative balancing weight for the eccentric weight. Find out relative weight for all eccentric weight and note down.

2)Dynamic balancing: -

From the relative weight (number of balls) assume position of two of the weights over shaft, draw the force polygon and find out position of other weights.

1) Mount the weights at proper position over the shaft.
2) Put the leather belt over the pulley and start the motor.
3) If the system is balanced, the shaft will rotate free from vibrations.

CALCULATIONS:

1) Static balancing: -

Let the given weights be m_1r_1 and m_2r_2 with an angle between them be m_3r_3 and m_4r_4 are the balancing weights whose angular position are to be determined. Draw positions of m_1r_1 and m_2r_2 in the position diagram. to draw force polygon draw AB parallel to m_1r_1 to some scale, from A, draw an arc whose radius is proportional to m_4r_4 and from C draw an arc with radius proportional to m_3r_3 the intersection of arc gives point D. Join AD and CD draw parallel lines to CD and AD in position diagram, this will give angular position of m_3r_3 and m_4r_4 respectively.

2) Dynamic balancing: -

Follow the procedure for static balancing of the system and find out angular position of balance weights. To find the linear position couple polygon is required, assume linear position of m_1r_1 taking moments about rotating plane of m_3r_3 couples are 1) m_1r_1x 2) $m_2r_2a_2$ 3) $m_4r_4a_4$

Draw 'ab' parallel to m_1r_1 to the scale of m_1r_1 couple. From 'b' draw parallel to m_2r_2 from 'a' draw parallel line to m_4r_4. The intersection gives point 'c'. "bc" is proportional to $m_2r_2a_2$ and "ac " is proportional to $m_4r_4a_4$. As m_2r_2 and m_4r_4 are known values of a_4 a_2 can be determined.

Calculation:

m_1 = 153.9 gr

m_2 = 151.3 gr

m_3 = 148.5 gr

m_4 = 147.2 gr

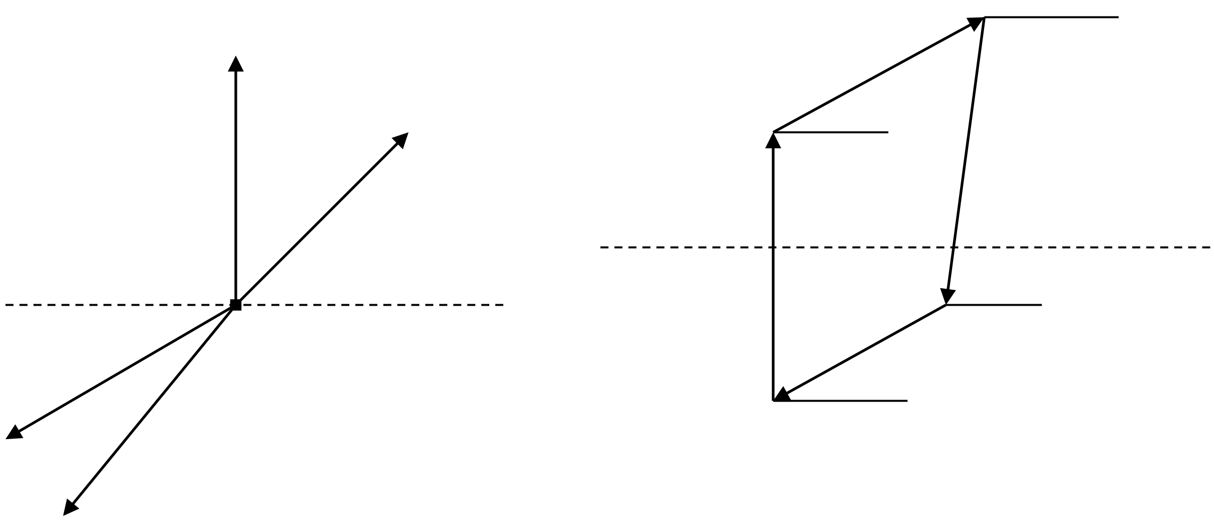
r_1 = 3.6cm

r_2 = 3.6cm

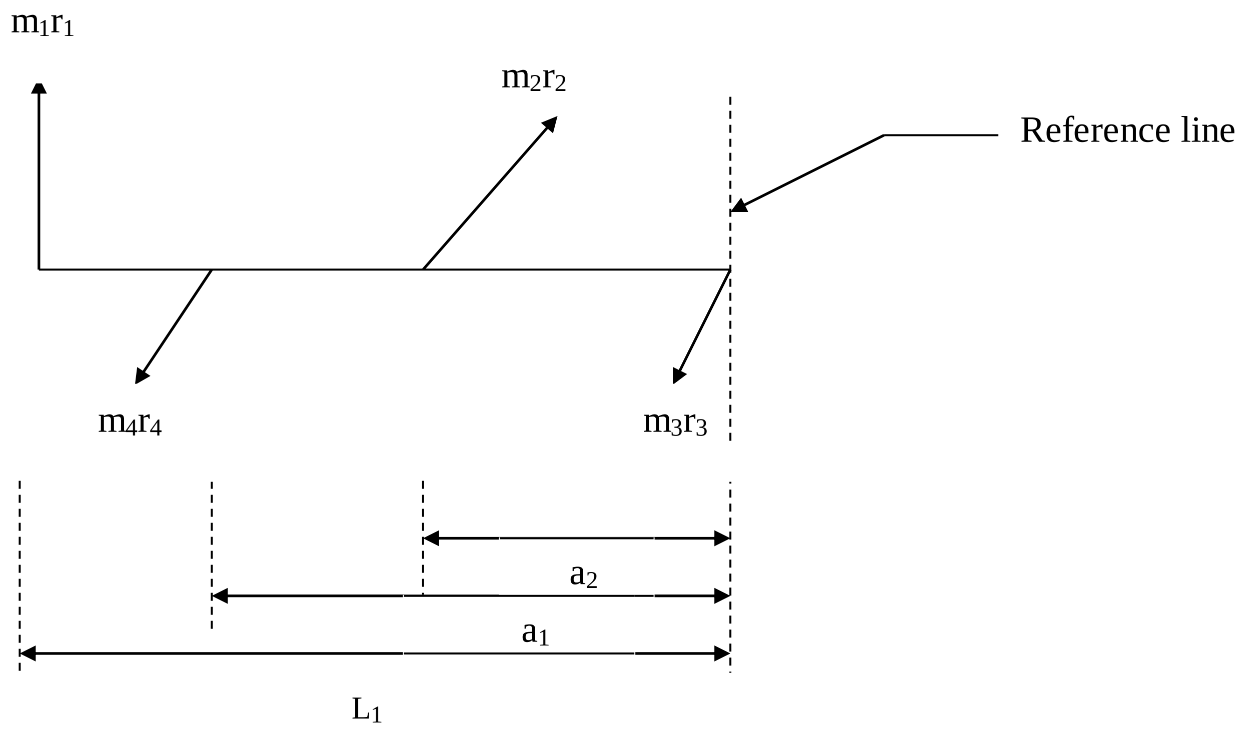
r_3 = 3.6cm

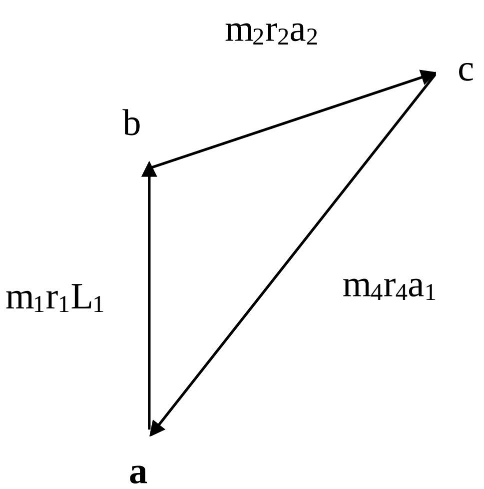
r_4 = 3.6cm

To find θ_3 and θ_4: -



TO FIND LINEAR POSITIONS :-





From graph

$m_2r_2a_2 =$ **'x'** mm

$\therefore a_2 =$ **x** $/ m_2r_2$

$m_4r_4a_1 =$ **'y'** mm

$\therefore a_1 =$ **'y'** $/ m_4r_4$

EXPERIMENT: 7
FREE UNDAMPED LONGITUDINAL VIBRATION OF SPRING MASS SYSTEM

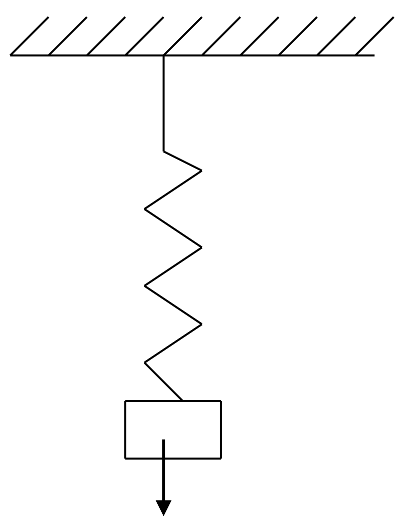
AIM: To study the undamped free vibration of the spring mass system

APPARATUS: Stopwatch, weights, and vernier scale.

PROCEDURE:

1. Fix the spring in the strut; attach the weight holder to the spring.
2. Fix the scale for measurement of elongation of spring at the suitable position. Note initial reading, attach different weights to the spring and note down the corresponding deflections.
3. Find out the stiffness of the spring 'K'
4. Repeat the experiments with different springs
5. Now, with weights attached to the spring set the spring vibrating and note down the time period.
6. Repeat the experiment with different springs and different weights.

EXPERIMENTAL SET UP:



FORMULAE:

δ = Deflection = final length – initial length.

K = stiffness of the spring = mg / δ

F_n (experi) = $1/t_p$

F_n (theo.) = $(1/2\Pi) * (\sqrt{K/m}) = (1/2\Pi) * (\sqrt{g/\delta})$

Where g = acceleration due to gravity in m/s^2

m = attached mass in kg

TABULAR COLUMN:

Sl.no	Attached mass in ‘kgs'	Deflection in ‘m’	Stiffness K in ‘N/m’	Time for In sec		Frequncy In ‘Hz’	
				10 osc	1 osc	Expi .	theo.
1	0.73	0.018	88.89	4.5	0.45	2.22	1.756
2	0.93	0.036	88.89	6	0.6	1.66	1.55
3	1.13	0.059	88.89	7	0.7	1.428	1.411
4							
5							

SPECIMEN CALCULATION:

Experimental frequency:

Fn=1/tp=1/.45=2.22Hz

Theoritical frequency:

$Fn=(1/2\Pi)*(\sqrt{K/m})=(1/2\Pi)*(\sqrt{88.89/0.73})=1.75Hz$

FROM GRAPH:

K=Force/unit deflection=1/0.0112=88.89N/M

EXPERIMENT NO.8
STRESS –CONCENTRATION FACTOR USING PHOTO- ELASTICITY

AIM: To determines stress concentration factor for a circular disc with a circular hole under diametrical compression.

APPARATUS: Circular Polariscope, photo elastic model in the form of circular disc with a circular hole, vernier caliper.

THEORY:

In the development of the basic stress equations for tension, compression, bending and torsion, it was assumed that no irregularities occurred in the member under consideration. But it is quite difficult to design a machine without permitting some changes in the cross-sections of the members.

Ex: rotating shafts must have shoulders designed on them so that the bearing can be properly sealed and so that they will take thrust loads. Other parts require holes, oil grooves and notches of various kinds.

Any discontinuity in a machine part alters the stress distribution in the neighborhood of the discontinuity so that the elementary stress equations no longer describe the state of stress in the part, such discontinuities are called stress raisers and the regions in which they occur are called areas of stress concentration.

Theoretical or geometric, stress-concentration factor k_t

It is the ratio of actual maximum stress at the discontinuity to the normal stress.

$k_t = \sigma_{max}/ \sigma_o$ $\quad$ $k_{ts} = \tau_{max} / \tau_o$

Where k_t used for normal stresses.

k_{ts} used for shear stresses.

The subscript t in k_t means that this stress- concentration factor depends for its value only on the geometry of the part. That is, the particular material used has no effect on the value of k_t .this is why it is called theoretical stress- concentration factor.

PROCEDURE:

1. The circular specimen is mounted between the lever arm which is extended from the fulcrum to the load acting on other side.the light emitted from sodium vapor lamp of circular polariscope is analyzed using both polarizes and analyzer.
2. The load is applied in the weight hanger and the fringe pattern is observed .the total number of integral formed plus the fractional fringes are counted and the fringe order is noted.
3. The load acting on the specimen is calculated. Repeat the procedure for various loads. At each load calculate the nominal and maximum stress acting on the specimen.
4. A graph is plotted b/w σ_{max} v/s σ_0 and the slope of this is obtained in order to calculate average value of stress concentration factor

SPECIMEN SPECIFICATIONS: -

- Outer diameter of specimen D = 70 mm
- Inner diameter of the specimen d = 28 mm
- Thickness of the specimen h = 5.23 mm
- Distance x = 410 mm
- Distance y = 1170 mm

Tabular column:

Sl.no	Load on hanger		Load on disc ‘P’ N	Fringe order N	σ_{act}	σ_{max}	K_σ
	Kg	N					
1	9	88.29	251.94	1.23	1.146	3.207	2.798
2	10	98.1	279.94	1.65	1.274	4.303	3.377
3	11	107.91	307.93	1.79	1.401	4.668	3.331
4							
5							
6							
7							

FORMULAE:

- Load on the disc
    - $P * x = w * y$
    - $P = wy/x$ in N
- $\sigma_{nom} = p / (D-d) h$ in N/mm^2
- $\sigma_{act} = N F_\sigma / h$ in N/mm^2
    - Where N= fringe order
- F_σ = Material fringe constant
- $K_\sigma = \sigma_{act} / \sigma_{nom}$

CALCULATION:

1.Load on the disc

i. $P * x = w * y$

ii. $P = w\ y/x = 88.29(1170)/410 = 251.94$ N

2. $\sigma_{nom} = p / (D-d)\ h = 251.94/(70.28)5.23$

$=1.146$ N/mm^2

3. $\sigma_{act} = N\ F_{\sigma} / h = 1.23(13.64)/5.23$

$= 3.207$ N/mm^2

4. $K_{\sigma} = \sigma_{act} / \sigma_{nom}$

$=3.207/1.146 = 2.798$

EXPERIMENT NO.9
FOUR POINT BENDING

AIM: - To calculate the bending stress of a beam using photo- elastic specimen.

APPARATUS: - circular polariscope, test specimen, weights and vernier caliper.

PROCEDURE: -

Place the specimen in the loading frame of the polariscope .the test specimen is supported as a beam, subjected to pure bending as a four pointing bending set-up, where load is applied in the weight hanger and the fringe pattern is observed. The total number of integral fringes formed plus the fractional fringes are counted. Repeat the procedure for various loads, at each load calculate the actual stress acting on the specimen and compare the actual stress with theoretical one.

SPECIFICATION:

For rectangular specimen:

- Height “H” = 23 mm
- Breath “B” = 6 mm
- Length “L” = mm
- Where “a” is the distance from the loading point to the reaction point = 20 mm
- Length “L_1” = 1430 mm
- “L_2” = 680 mm
- “L_3” = 630 mm
- Diameter “d” = mm.

FORMULAE:

- Actual stress = σ_{act} = N F_σ / h = N/mm^2

  Where N is fringe order

  F_σ is Material fringe constant.

- Theoretical stress σ_{theo} = 6* P * a / b H^2

TABULAR COLUMN:

Sl no	Load in hanger		Load on specimen 'P' N	Fringe order	σ_{act} N/mm^2	σ_{theo} N/mm^2
	Kg	N				
1	5	49.07	107.08	4.048	1.727	0.76
2	7	68.67	149.92	5.688	2.657	1.17
3						
4						

CALCULATION:

a) Load on specimen

$2WL_1 = PL_2 + PL_3$

P = 2(49.07) 1430/(680+630)

= 107.08 N

b) σ_{theo} = 6* P * a / b h^2

σ_{theo} = $6(107.08)20/6(23)^2$

= 4.408 N/mm^2

c) σ_{act} = N F_σ / h

= 0.76(13.64)/6

= 1.727 N/mm^2

EXPERIMENT NO.10

CALIBRATION OF PHOTO- ELASTIC MATERIAL USING A CIRCULAR DISC UNDER COMPRESSION (DIAMETRICAL –COMPRESSION)

AIM: To determines the material and model fringe constant, using photo elastic material under diametrical compression

APPARATUS: photo-elastic apparatus with polarizes analyzer and photo elastic specimen.

PROCEDURE:

The circular disc is mounted between the lever arms, which is extended from the fulcrum to the load acting on the other side. The light emitted from the sodium vapor lamp of the circular polariscope is analyzed using both polarizes and analyses. This setup is set dark field and then the load is applied in the weight hanger. This exerts a pressure on the disc at the vertical edge and the fringe pattern appears which can be seen through the analyzer.

The analyzer is rotated till the emerging fringe at the edge coincides with the clearly formed fringe at the center of the specimen. The angle of rotation and the fringe order is determined. Repeat the experiment for different loads on the pan and determine various parameters. The fractional fringes are compensated by Tardy's compensation method. The analyzer is turned in clockwise or counterclockwise to move the fringe from lower to higher order or vice versa, until the fringe coincides and separate and the angle turned is noted.

Case1: - Fringes move from higher order to lower order.

The total number of fringes = number of Integral fringes – angle turned /180^0

Case 2: - when the fringes move from lower to higher order

The total number of fringes = number of Integral fringes + angle turned /180^0

A graph is plotted between P v/s N and the slope of is obtained in order to calculate material and fringe constant.

SPECIFICATION:

Diameter 'D' = 70 mm

Thickness 'h' = 6 mm

Length 'L_1' = 780 mm

'L_2' = 329 mm

TABULAR COLUMN:

Sl.no	Weight applied		Load acting on specimen 'p' in N	Fringe order
	Kg	N		
1	5	49.05	165.29	(1–0.52)=0.48
2	7	68.67	231.41	(1-0.37)=0.63
3				
4				
5				

FORMULAE:

a) Load acting on specimen

$W_1 * (L2 + L_1) = P * L_2$

b) Material fringe constant:

$F_\sigma = (P / N) * (8/ 3.14 * D)$ N / mm –Fringe

Where P=Load acting on specimen

N=Fringe order

D=Diameter of specimen

c) Model Fringe constant: -

$f_\sigma = F_\sigma / h$ in mm

CALCULATION:

a) Load acting on specimen:

$W_1 * (L2 + L_1) = P * L_2$

$P = 49.05(329+780)/329$

$= 165.29$ N

b) Material fringe constant:

$F_\sigma = (P / N) * (8/ 3.14 * D)$

$=(66.12/0.17)*(8/3.14*70)$

$= 14.15$ N / mm –Fringe

c) Model Fringe constant:

$f_\sigma = F_\sigma / h = 14.15/6$

$=2.358$ N/mm^2 /fringe

EXPERIMENT NO.11

FORCED DAMPED VIBRATION OF SPRING MASS SYSTEM USING CANTILEVER

AIM: - To study forced damped vibrations of spring mass system using cantilever beam.

APPARATUS: -Spring, beam, Damper, Exciter

PROCEDURE: -

1. Attach the vibration recorder at suitable position so that pen attached to the pen holder is lightly pressing over the paper
2. Attach the damper over the beam and spring to the stud. Set the damper at minimum damping positions.
3. Start the vibration recorder.
4. Increase the speed and again read the vibration.
5. At resonance speed the amplitude of vibration may cross the width of paper. Hold the system and take few reading at speed higher then the resonance speed.
6. Noting down the frequency of recorder of the vibration. Repeat the experiment for different level of damping.

FORMULAE:

a) **Angular velocity,**

$\omega = (\omega_1 + \omega_2)/2$

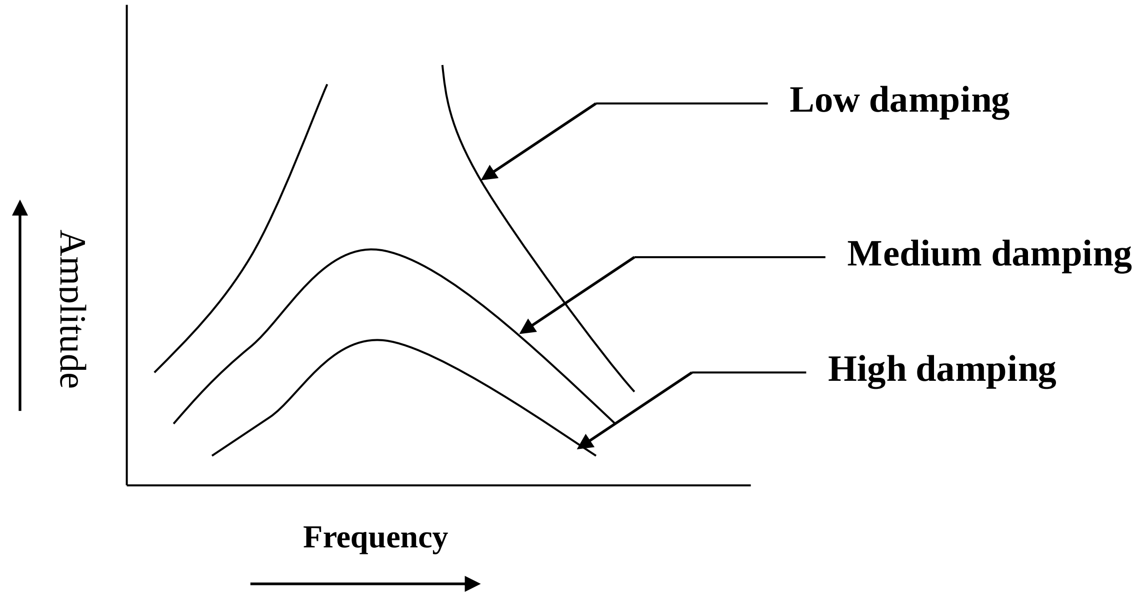
b) **Damping ratio,**

$\xi = (\omega_2 - \omega_1)/2\ \omega$

TABULAR COLUMN: -

Sl.no	Damping position	Speed in ‘rpm’ N	Amplitude in ‘mm’	Frequency ‘Hz’	
				Theo. (N/60)	Graph
1	Full close	550	1.25	9.166	
2	Three- fourth (3/ 4)				
3	Half (1/ 2)				
4	One –fourth (1 /4)				

GRAPH: -


Low damping
Medium damping
High damping
Amplitude
Frequency

EXPERIMENT NO.12
GYROSCOPE

AIM: To find the angular velocity of precision.

APPARATUS: Stop clock, gyroscope tachometer, Weights.

PROCEDURE:

1. Check the rotor for vertical position
2. Adjust the balance weights slightly if necessary
3. Keep the dimmer stat at required position
4. Start the motor by applying the voltage
5. Adjust the speed as required
6. Note down the rotor speed with help of tachometer
7. Speed is noted at steady state
8. Put the weights on the stud & at the same time start the stop clock & note down the time for $45^0/90^0$
9. Repeat the experiment for different weights & speed

SPECIFICATION:

- Mass of Rotor M = 3.81 Kg
- Diameter of rotor d = 0.25 m
- Distance between weights stud & center of disc = 0.25m
- Mass moment of inertia of disc $I = mr^2/2 = 0.0297$ kg.m^2

FORMULAE:

1) Angular velocity of disc $\omega = 2\pi N/60$
2) Angular velocity of precision $(\omega_p)_{exp}$ = angle turned / time taken
3) Angular velocity of precision $(\omega_p)_{theo} = M_t/I\omega$

TABULAR COLUMN:

			Time taken for angle turned		Velocity of precision	
Sl no	Rotor Speed 'N' rpm	Mass added in 'Kg'	Angle 'θ'	Time 'sec'	$(\omega_p)_{exp}$ rad/s	$(\omega_p)_{theo}$ rad/s
1	3000	0.2	45^0	26	0.0302	0.0524
2	3000	0.5	90^0	17	0.0923	0.1337

CALCULATIONS:

1) Angular velocity of disc $\omega = 2\pi N/60$

$= 2x\ \pi\ x\ 3000\ /60$

$= 314.159$ rad/ s

2) Angular velocity of precision $(\omega_p)_{exp}$ = angle turned / time taken

$= 45/26 = 0.0302$ rad/s

3) Angular velocity of precision $(\omega_p)_{theo} = M_t/I\omega$

$= 0.2\ x\ 9.81\ x\ 0.25\ /\ 0.0297\ x\ 314.159$

$= 0.0524$ rad/ s

EXPERIMENT NO.13
SLIDER BEARING

AIM: To find the pressure distribution over the bearing.

APPARATUS: slider bearings, apparatus, Manometer.FillerGauge, Tachometer & thermometer.

PROCEDURE:

1. Motor is connected to the supply
2. The oil of required viscosity is filled in the tank to a particular level such that lower part of the belt is completely immersed in oil.
3. The tilting pad is adjusted with the help of chuck nut & filler gauge to get the required value of 'n' by adjusting h_0 & h_1
4. The motor is started & speed is gradually raised till we get required speed of shaft, which is connected to the motor by a V-belt drive
5. The readings for pressure head in all the tubes is measured only after the equilibrium condition has reached, at this time oil temperature should be noted down to get exact value of viscosity
6. Keeping h_0 & h_1 same pressure heads for different speeds are noted.

SPECIFICATION & OBSERVATION:

- Length of the driven pulley L = 137 mm
- Width of the belt B = 120 mm
- Diameter of roller D = 112 mm
- Grade of oil used = SAE 40
- Oil film thickness at entry side h_1 = 3mm
- Oil film thickness at exit h_0= 2mm
- Speed N = 280 rpm
- Density of oil = 853kg/m^3
- Viscosity of oil at 32^0c = 0.283 N-S/m^2

FORMULAE:

1) Pressure $p = 6\eta VL/ h_0^2 \{ (nX/L) (1-X/L) / (2+ n)(1+nX/L)^2 \}$ N/m$^{2]}$

Where $n = (h_0 / h_1) -1$

X = tapping distance in mm

η = Viscosity of the given oil

$V = \pi DN /60$ N = speed of the driven pulley

2) Theoretical oil film thickness $h_{theo} = p/\rho g$

Where ρ = density of the oil

g = acceleration due to gravity

3) Load carrying Capacity $W = 6\eta VBC_1/k^2$

Where $C_1 = \ln(a-k/a) + (2k/2a-k)$

$k=(h_0 - h_1) /B$

$a = h_0 /B$

4) Frictional force = ηVLC_2

Where $C_2 = (-4/k) \ln(a-k/a) - (6/2a-k)$

5) Co efficient of friction = F/ w

TABULAR COLUMN:

Longitudinal tapings

Taping no	$h_{pratical}$ in ‘m’	h_{theo} in ‘m’	Pressure in ‘N/m^2	Taping distance X in ‘m’
1	0.07	0.173	1448.4	0.0125
2	0.27	0.296	2477.31	0.0265
3	0.49	0.36	3018.57	0.0405
4	0.67	0.38	3183.03	0.0545
5	0.79	0.365	3055.77	0.0685
6	0.63	0.322	2702.66	0.0825
7	0.57	0.259	2175.04	0.0965
8	0.5	0.18	1513.13	0.1105
9	0.43	0.094	748.65	0.1245

Transverse tapings

Taping no	$h_{pratical}$ in ‘m’	h_{theo} in ‘m’	Pressure in ‘N/m^2
A	0.28	0.26	2175
B	0.41	0.26	2175
C	0.46	0.26	2175
D	0.49	0.26	2175
E	0.515	0.26	2175
F	0.525	0.26	2175
G	0.52	0.26	2175
H	0.51	0.26	2175

EXPERIMENT NO.14
JOURNAL BEARING

AIM: To determine the pressure distribution in the oil film of the bearing for various speeds & plot the Cartesian & polar pressure curve for various speeds

To determine the constants 'n' & 'k'& plot the sommerfield pressure curve for each speed.

APPARATUS: Journal bearing apparatus, dimmer stat, Tachometer, Dc motor, manometer counter balance& weights.

PROCEDURE:

1. fill the oil tank using required SAE grade oil under test & position the tank at the desired level
2. drain out the air from all the tubes of the manometers & check level balance with the supply level.
3. check for any leakage of the oil.
4. Some leakage of the oil is necessary for cooling purpose
5. Check the d9irection of rotation & increase the speed of motor slowly.
6. Set the speed & let the journal run for about 30 minutes. until the oil in the bearing is warmed up
7. Check the steady oil level at various tappings.
8. Add required load & keep the balancing load in horizontal position & observer the steady level.
9. When the manometer level settler down to steady level take the pressure readings of 16 manometer tubes
10. Repeat the experimental for various speeds & constant loads or constant speed & varying load.

SPECIFICATION & OBSERVATION:

- Diameter of journal d = …….mm
- Length of journal L = …….mm
- Diameter of bearing D =…….mm
- Speed of the motor = …….. rpm
- Hanger Weight = ……N
- Total weight = ………N
- Initial Pressure P_0 …….N /m^2

TABULAR COLUMN :

Manometer	Pressure P N /m^2	Pressure Diff P- P_0 N /m^2
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
A		
B		
12		
C		
D		

FORMULAE :

Pressure distribution in Journal

$(P - P_0)_{max} = -K \sin\theta(2+\varepsilon \cos \theta) / (1+ \varepsilon \cos \theta)^2$

i. Find K = ……….

Where θ_{max} = ……. Get the value from the Graph

ii. $\cos\theta_{max} = -3 \varepsilon / (2+\varepsilon^2)$

iii. Get ε …. From the above Equation

Load Carried by oil in the projected area

iv. $W = h\rho dL$

Where Avg Film Thickness h = sum of $(P - P_0)$ / number of positive Value

Theoretical Load $w = \{(12 \eta r^3\omega\pi)/ \delta\} X (\varepsilon / 2+\varepsilon^2) X \{1/\sqrt{(1-\varepsilon^2)}\}$

Where δ = Radial clearance = D-d/2

Frictional Couple $M = \{(4 \eta r^3\omega\pi)/ \delta\} X (1+2\varepsilon^2 / 2+\varepsilon^2) X \{1/\sqrt{(1-\varepsilon^2)}\}$

Frictional Force $F = (2 \eta NLd\pi^2)/ \psi$

b. coefficient of friction $\mu = F/w$

EXPERIMENT NO.15
STRESS CONCENTRATION USING STRAIN GAUGE

AIM: To determine the stress concentration factor at a point near a semicircular notch in a brass plate subjected to tension.

APPARATUS: Brass plate model, strain indicator, spring balance, hooks loading frame strain gages (foil type)

PROCEDURE:

1. Connect the strain indicator to the strain gage o/p cable & to the A.C.mains
2. Fix the brass model to the loading frame using spring balance & hooks to the loading frame
3. Switch on the supply with no load
4. Calibrate the digital indicator for all strain gages using appropriate knobs to read zero
5. Load the model using loading screw & note the gage o/p in μ volts
6. Repeat this for different loading.

SPECIFICATION:

- Young's modulus of brass plate E = ……….N/m^2
- Width of the model w = ……..m
- Thickness of the model t = ……….m
- Notch radius a = ……..m

FORMULAE:

- Strain ε = bridge out put /gage factor
- $\sigma_{max} = \varepsilon E$
- σ_{nom} = load /(W-a)t

TABULAR COLUMN:

	δE Volts				ε				σ_{max}					k_t			
Load in Kg	1	2	3	4	1	2	3	4	1	2	3	4		1	2	3	4

VIVA QUESTIONS

1. Classify bearings?
2. What is the difference between hydrodynamic and hydrostatic bearing?
3. Sketch the variation of pressure in the converging film in journal bearing?
4. What are the properties of bearing material?
5. What are the properties of lubricant?
6. Differentiate dynamic and kinematic viscosity?
7. What is bearing characteristics number?
8. Plot the variation of coefficient of friction with bearing characteristics and identify the important regions?
9. What is the summerfield number?
10. At very high speed which one is preferred –journal or ball bearing?
11. Discuss pressure distribution in journal bearing?
12. Express state of strain at any point on the free surface of a body using Cartesian co-ordinate?
13. How strain gauges are are classified?
14. What are the main advantages of electric resistance strain gauges?
15. What are the applications of strain gauges?
16. Define strain sensitivity of a strain gauges?
17. How strain gauges rosettes are specified? Give example
18. Write basic torque equation and give an expression for shear stress?
19. Write basic bending equation and give an expression for bending stress?
20. Give expressions for principal stresses in terms of Cartesian stresses?
21. Give expressions for principal strain in terms of Cartesian strain?
22. What is the nature of light?
23. Define wave front, disturbance?
24. What are the requirements of a photo elastic material?
25. Name few of the photo elastic material.

26. What is polari scope? How many types are there?
27. What is polarizer?
28. what is the difference between polarizer and analyzer.
29. What is a fringe order? What do you understand birefrigerent materials. Can you name few such materials?
30. What is a fringe constant?
31. What is a wave plate how are they classified?
32. What are the advantages of photo elasticity over other experimental techniques?
33. What is meant by polarized light?
34. What are the elements of circular polariscope?
35. What is meant by polarizer, analyzer, quarter wave plate, half wave plate?
36. How can we produce dark field and bright field arrangement using circular polariscope.
37. Difference between isochromatics and isoclinics.
38. What are the methods used for determining the fractional fringe order.
39. What is scattered light photo elasticity?
40. Explain oblique incidence method.
41. Explain why stress concentration occurs at inner fiber of curved beams.
42. What is fringe Multiplication factor?